

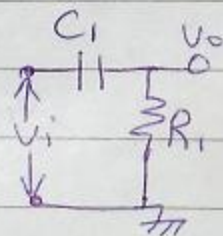
CHAPTER 2

Freqy Response

2.1 Low freqy Response

$$V_o(s) = \frac{R_1}{R_1 + 1/sC_1} V_i(s)$$

$$\therefore V_o(s) = \frac{s}{s + 1/R_1C_1} \cdot V_i(s)$$



$$\therefore AL(s) = \frac{s}{s + 1/R_1C_1} = \text{T.F.} \quad \text{Where } s = j\omega = j2\pi f$$

- * This function has zero when $s=0$
- * This function has pole when $s = -1/R_1C_1$
- * For Real freqy $s = j\omega = j2\pi f$

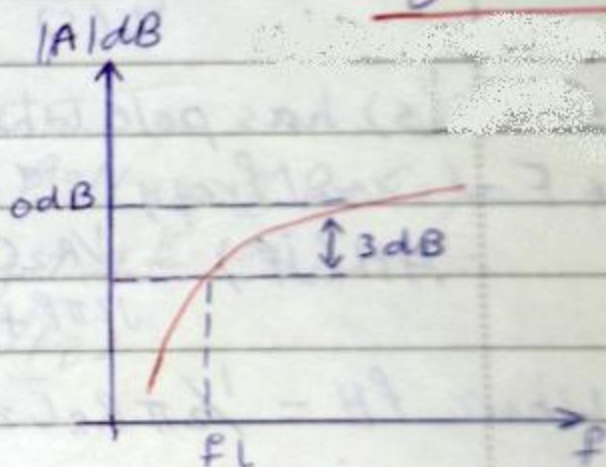
$$\therefore AL(jf) = \frac{j2\pi f}{j2\pi f + 1/R_1C_1} = \frac{1}{1 - j(fL/f)}$$

* Where: $f_L = \frac{1}{2\pi RC_1} \Rightarrow$ lower 3dB freq.

$$\sim |A_L(jf)| = \frac{1}{\sqrt{1 + (f_L/f)^2}}, \theta = \tan^{-1}(f_L/f)$$

* $f = f_L \rightarrow |A_L| = \frac{1}{\sqrt{2}} = 0.707 \rightarrow$ mid band region

So f_L is a freq at which the gain has fallen to 0.707 times the mid band value A_0 .

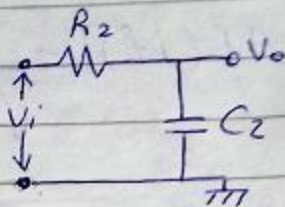


In (dB) $\rightarrow 20 \log \frac{1}{\sqrt{2}} = 3\text{dB}$, so f_L is the lower 3dB freq.

2.2 High freqy Response.

$$V_o(s) = \frac{1/sC_2}{1/sC_2 + R_2} \cdot V_i(s)$$

$$V_o(s) = \frac{1/R_2 C_2}{s + 1/R_2 C_2} \cdot V_i(s)$$



$$\therefore A_H(s) = \frac{V_o(s)}{V_i(s)} = \frac{1/R_2 C_2}{s + 1/R_2 C_2} = \text{T.F}$$

* $A_H(s)$ has pole when $s = -1/R_2 C_2$

zero لا يوجد
قطب يوجد

* For real freqy $s = j\omega = j2\pi f$

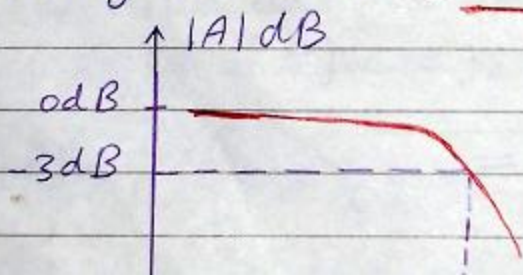
$$\therefore A_H(jf) = \frac{1/R_2 C_2}{j2\pi f + 1/R_2 C_2} = \frac{1}{1 + jf/f_H}$$

Where $f_H = 1/2\pi R_2 C_2 \Rightarrow$ upper 3dB freqy

$$|A_H(jf)| = \frac{1}{\sqrt{1 + (f/f_H)^2}}, \quad \theta_H = \tan^{-1}(f/f_H)$$

Also At $f = f_H$ the gain reduced to $1/\sqrt{2}$ its mid band then f_H is called upper 3dB freqy.

* The freqy dependence c/s on high and low freqy range is called (Bode plot)



2.3 Bode plot

* The freq Response is indicated by two curves:

- ① The magnitude of T.F.
- ② The phase Angle of T.F.

These two curves may be approximated by piece wise linear regions.

2.3.1 Single pole T.F.

Consider $A(s) = A_0 / (1 + s R_2 C_2)$
for real freq $s = j 2 \pi f$ then

$$A(jf) = A_0 / (1 + j f/f_p)$$

Where $f_p = 1/2\pi R_2 C_2$

$$|A| = \frac{|A_0|}{\sqrt{1 + (f/f_p)^2}}, \quad \theta = -\tan^{-1} f/f_p$$

$$|A|_{dB} = \underbrace{20 \log |A_0|}_{\downarrow} - 20 \log \sqrt{1 + (f/f_p)^2}$$

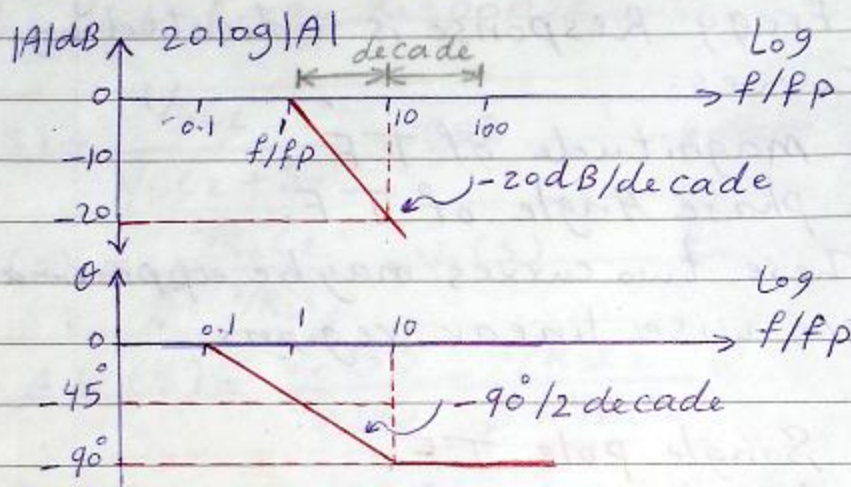
* for $f < f_p \rightarrow$ The c/s is horizontal line

* for $f > f_p \rightarrow$ The c/s is straight line of slope
-20 dB per decade

* for $f \ll f_p \rightarrow$ then $\theta \rightarrow 0^\circ$ OR at $f = 0.1 f_p$
 $\rightarrow \theta = 0^\circ$

* for $f \gg f_p \rightarrow$ then $\theta \rightarrow -90^\circ$ OR at $f = 10 f_p$

* For $f = f_p \rightarrow \theta = -45^\circ$.



For phase Angle when $0.1 f_p < f < 10 f_p$ we plot a straight line of slope of $-90^\circ/2 \text{ decade}$.

33.2: Single Zero T.F.

Consider $A(s) = A_0(1 + sK)$ then
 $A(jf) = A_0(1 + j f/f_z)$, $f_z = 1/2\pi K$
 $|A|_{dB} = 20 \log |A_0| + 20 \log \sqrt{1 + (f/f_z)^2}$
 $\theta = \tan^{-1} f/f_z$
 $K = \text{constant}$

